

Mécanique des Fluides Compressibles

Méthode des caractéristiques

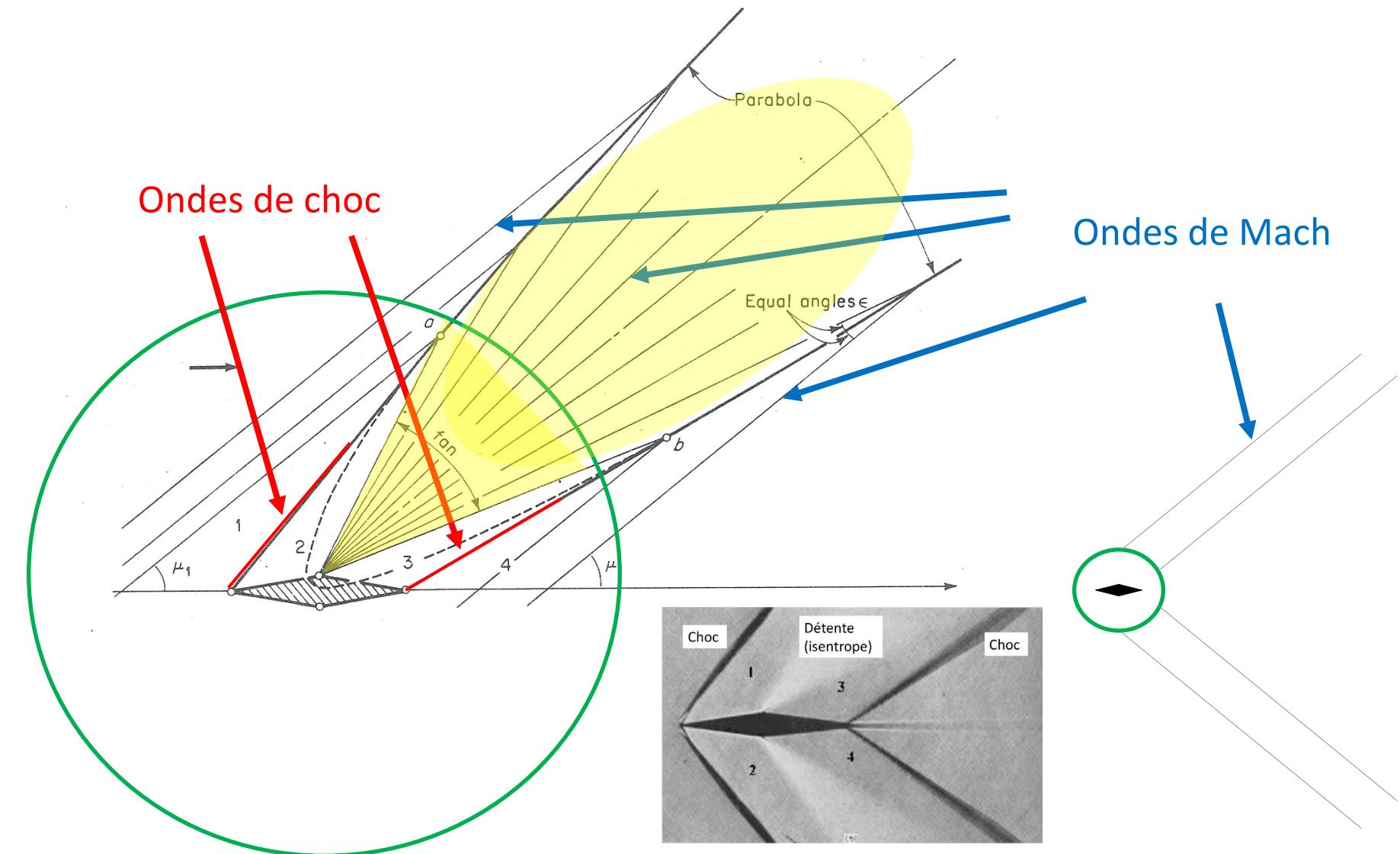
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Semestre printemps 2024-2025

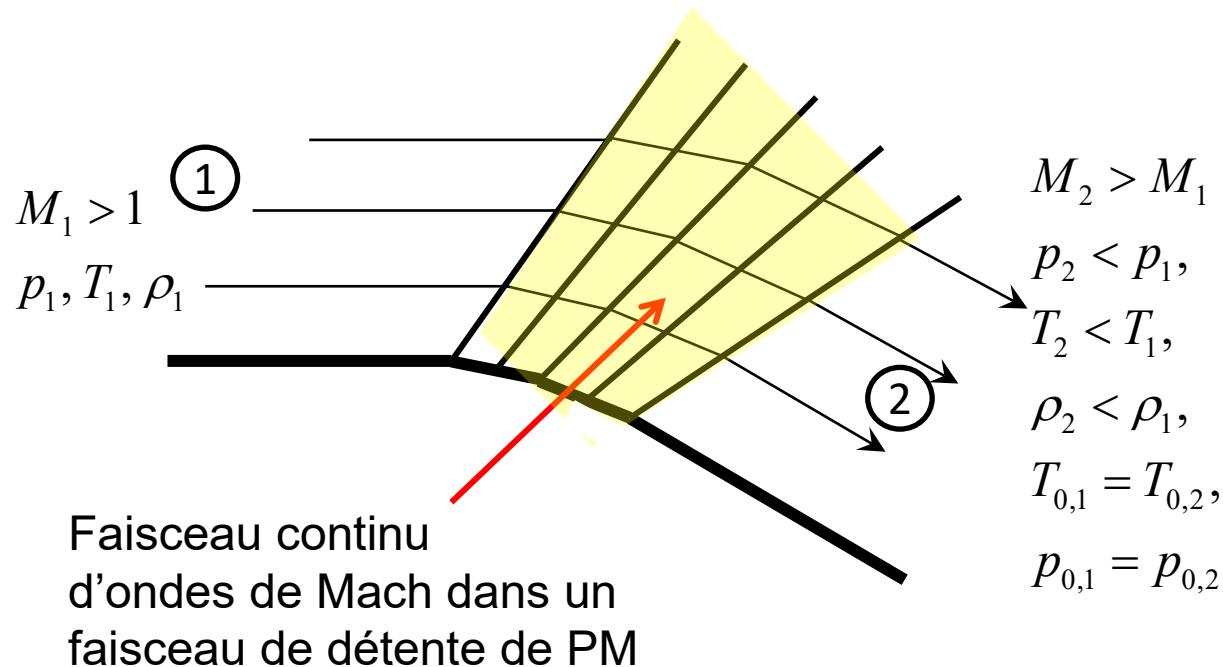
Exemples

Ondes de choc

Ondes de Mach

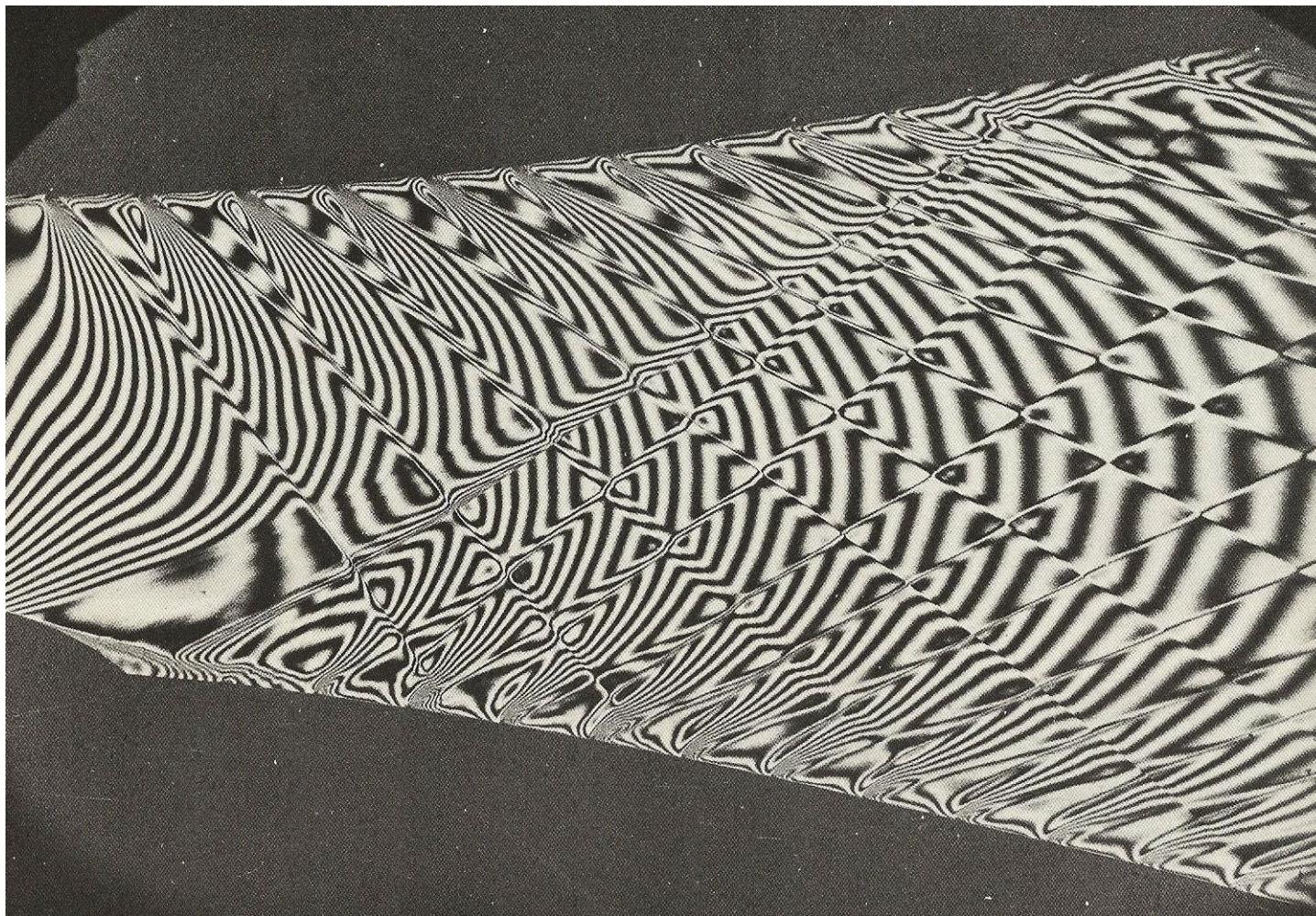


Exemples



Exemples

EPFL



➤ Hypothèses:

- Ecoulements supersoniques
- Bidimensionnels
- Stationnaires
- Homentropiques (entropie uniforme)
- Enthalpie totale uniforme
- Irrotationnels
- Pas de forces volumiques extérieures

➤ Conservation de la masse: $\nabla \cdot (\rho \mathbf{u}) = 0$

➤ Conservation de la quantité de mouvement par la loi de Crocco:

$$\nabla \left(\frac{\mathbf{u}^2}{2} \right) - \mathbf{u} \times \boldsymbol{\omega} = -\frac{1}{\rho} \nabla p$$

$$-\mathbf{u} \times \boldsymbol{\omega} + \nabla h_0 = T \nabla s$$

$$dh = Tds + vdp$$

$$\left(\frac{\partial \mathbf{u}}{\partial t} - \mathbf{u} \times \boldsymbol{\omega} \right) = -\nabla h_0 + T \nabla s + \mathbf{f}$$

➤ Conservation de l'énergie

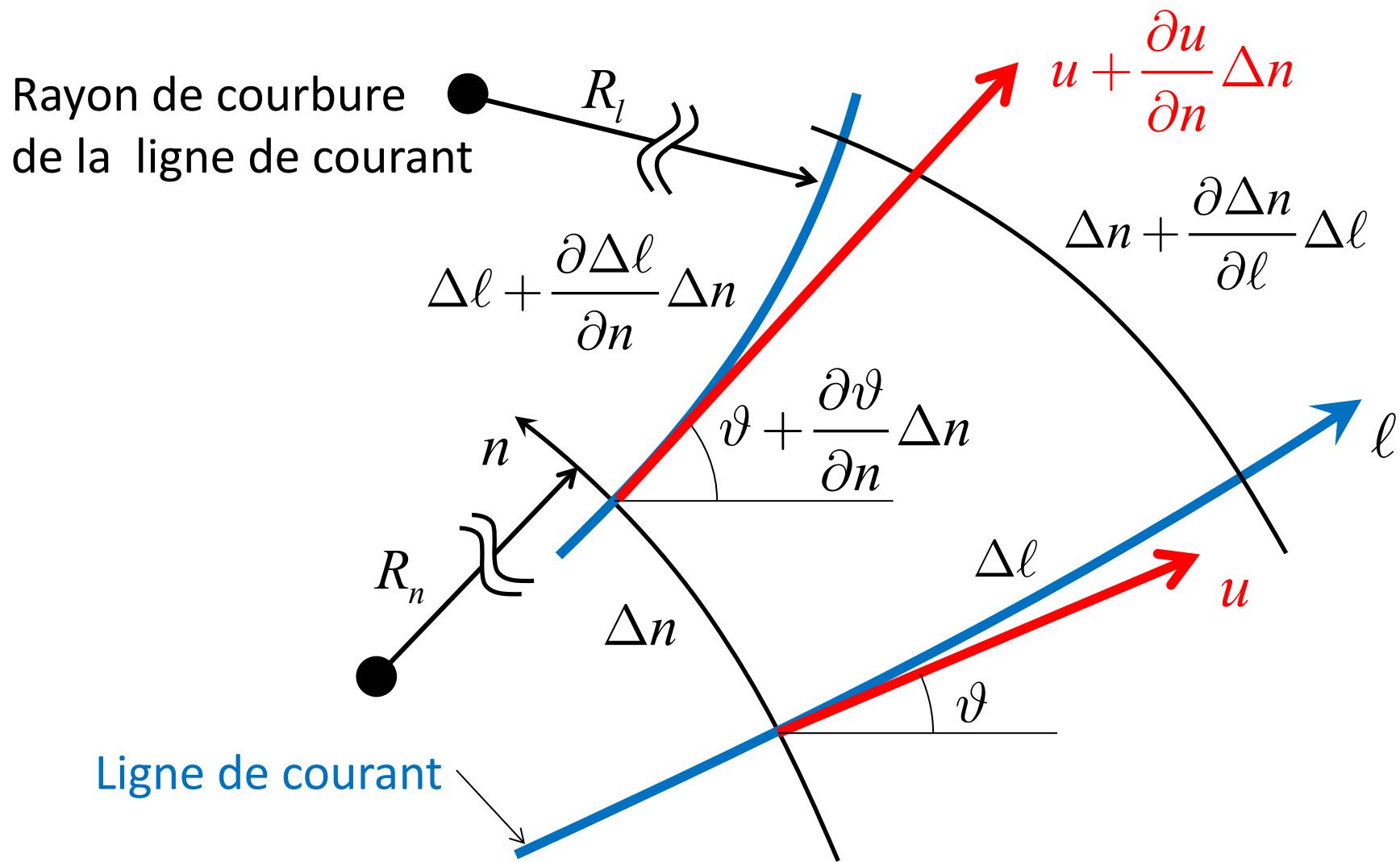
$$\mathbf{u} \cdot \nabla h_0 = 0$$

$$\mathbf{u} \cdot \nabla s = 0$$

- On ne considérera que des écoulements **irrotationnels** $\boldsymbol{\omega} = \nabla \times \mathbf{u} = 0$
- L'entropie est choisie comme étant UNIFORME = écoulement **homentropique**
- L'enthalpie totale est choisie comme étant **UNIFORME**
- Deux de ces conditions impliquent l'autre, car:

$$-\mathbf{u} \times \boldsymbol{\omega} + \nabla h_0 = T \nabla s$$

- Hypothèses valables, faites jusqu'à présent (avec les ondes de chocs, l'entropie était uniforme en amont et en aval du choc)
- **Hors des couches limites** ou des sillages
- **Pas de chocs courbes**



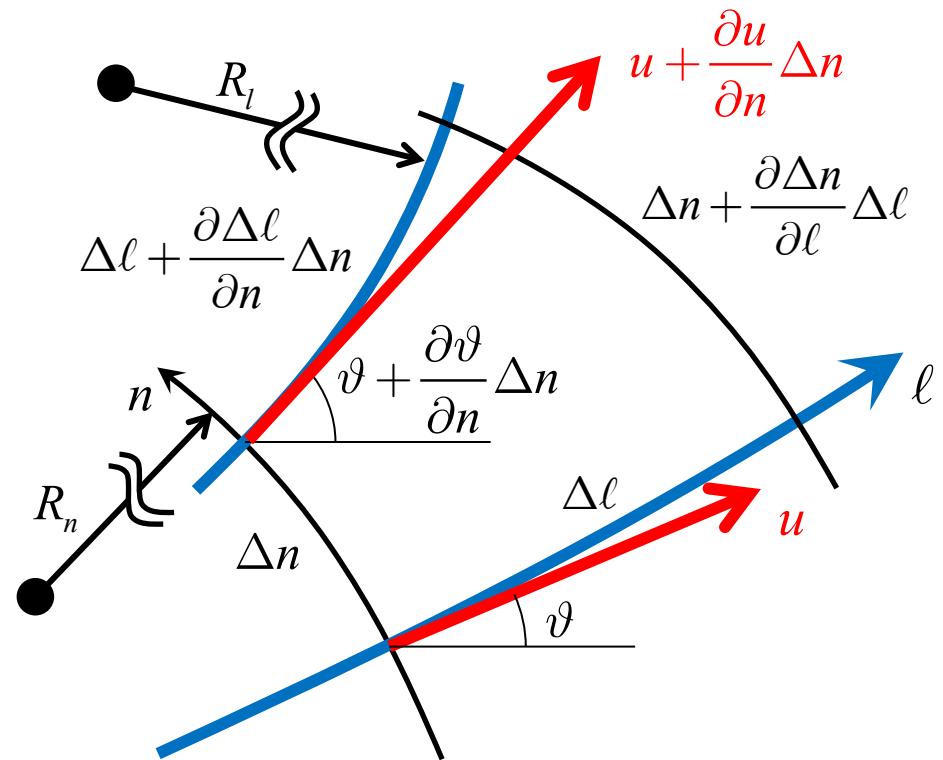
- Coordonnées «naturelles», basées sur les lignes de courant
- Vecteur vitesse défini par le module de sa vitesse u et son angle ϑ

$$u, \vartheta$$

$$u^2 = \mathbf{u} \cdot \mathbf{u}$$

$$\frac{1}{R_n} = \frac{1}{\Delta n} \frac{\partial \Delta n}{\partial \ell} = \frac{\partial \vartheta}{\partial n}$$

$$\frac{1}{R_l} = -\frac{1}{\Delta \ell} \frac{\partial \Delta \ell}{\partial n} = \frac{\partial \vartheta}{\partial \ell}$$

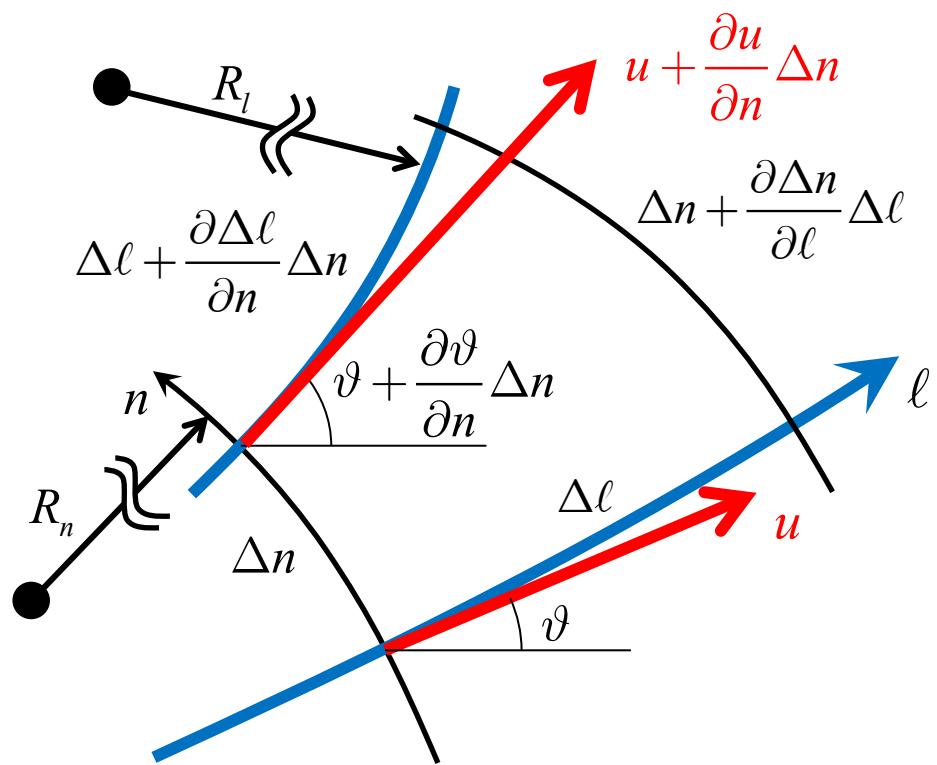


➤ Conservation de la masse

$$\rho u \Delta n = const$$

➤ Dérivée logarithmique

$$\frac{1}{\rho} \frac{\partial \rho}{\partial \ell} + \frac{1}{u} \frac{\partial u}{\partial \ell} + \frac{\partial \vartheta}{\partial n} = 0$$



$$\left| \frac{1}{\Delta n} \frac{\partial \Delta n}{\partial \ell} \right| = \frac{\partial \vartheta}{\partial n} \quad \left(= \frac{1}{R_n} \right)$$

- Conservation de la quantité de mouvement **selon la ligne de courant**

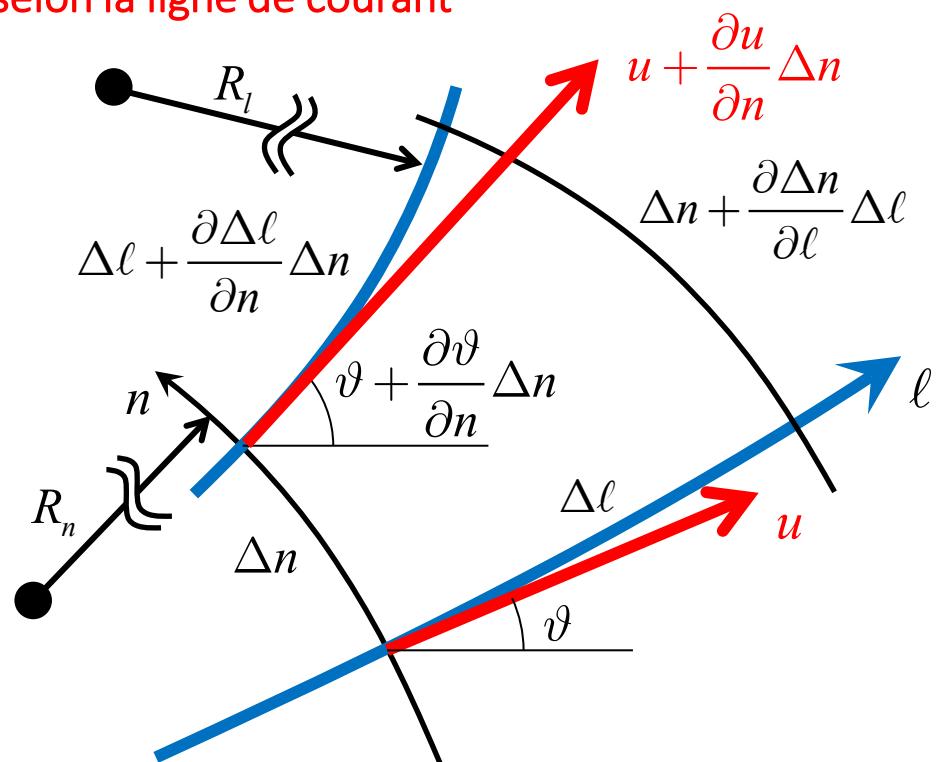
$$u \frac{\partial u}{\partial \ell} = -\frac{1}{\rho} \frac{\partial p}{\partial \ell}$$

➤ Or $dp = a^2 d\rho$

$$u \frac{\partial u}{\partial \ell} = -\frac{a^2}{\rho} \frac{\partial \rho}{\partial \ell}$$

- Avec conservation de masse

$$(M^2 - 1) \frac{1}{u} \frac{\partial u}{\partial \ell} - \frac{\partial \vartheta}{\partial n} = 0$$



$$\frac{1}{\rho} \frac{\partial \rho}{\partial \ell} + \frac{1}{u} \frac{\partial u}{\partial \ell} + \frac{\partial \vartheta}{\partial n} = 0$$

Irrotationalité

➤ Théorème de Stokes

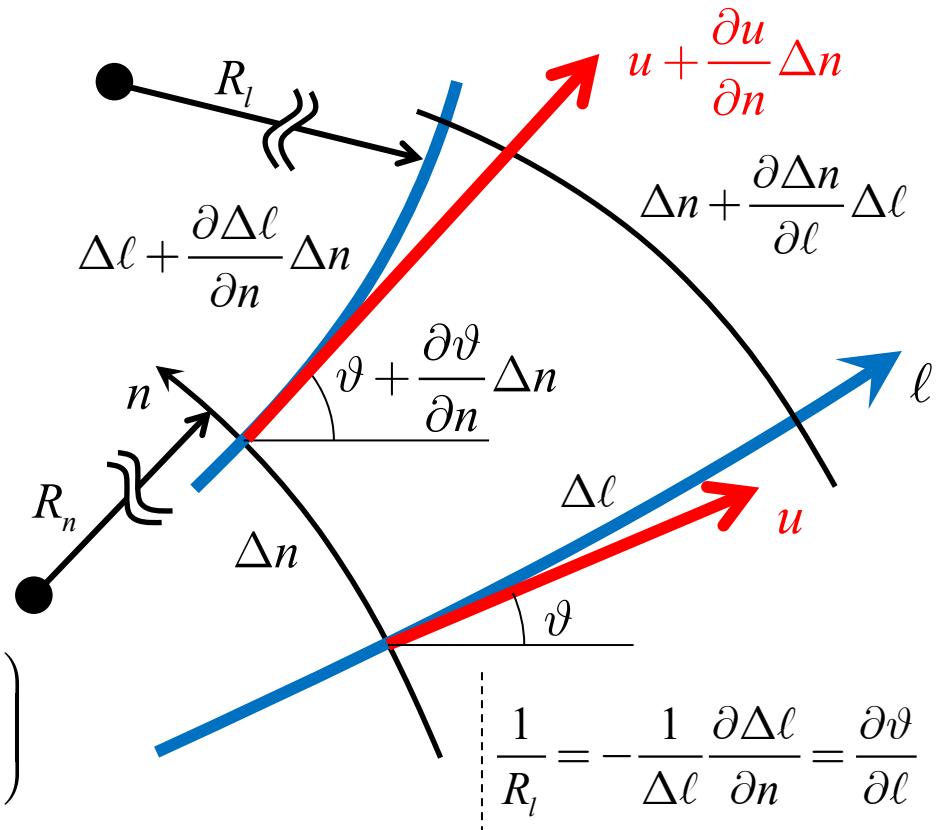
$$\iint \omega dS = \oint \mathbf{u} \cdot d\mathbf{x}$$

$$\iint \omega dS \sim \omega \cdot \Delta n \cdot \Delta \ell$$

$$\iint \omega dS$$

$$\sim u \Delta \ell - \left(u + \frac{\partial u}{\partial n} \Delta n \right) \left(\Delta \ell + \frac{\partial \Delta \ell}{\partial n} \Delta n \right)$$

$$\omega = - \frac{\partial u}{\partial n} + u \frac{\partial \vartheta}{\partial \ell}$$

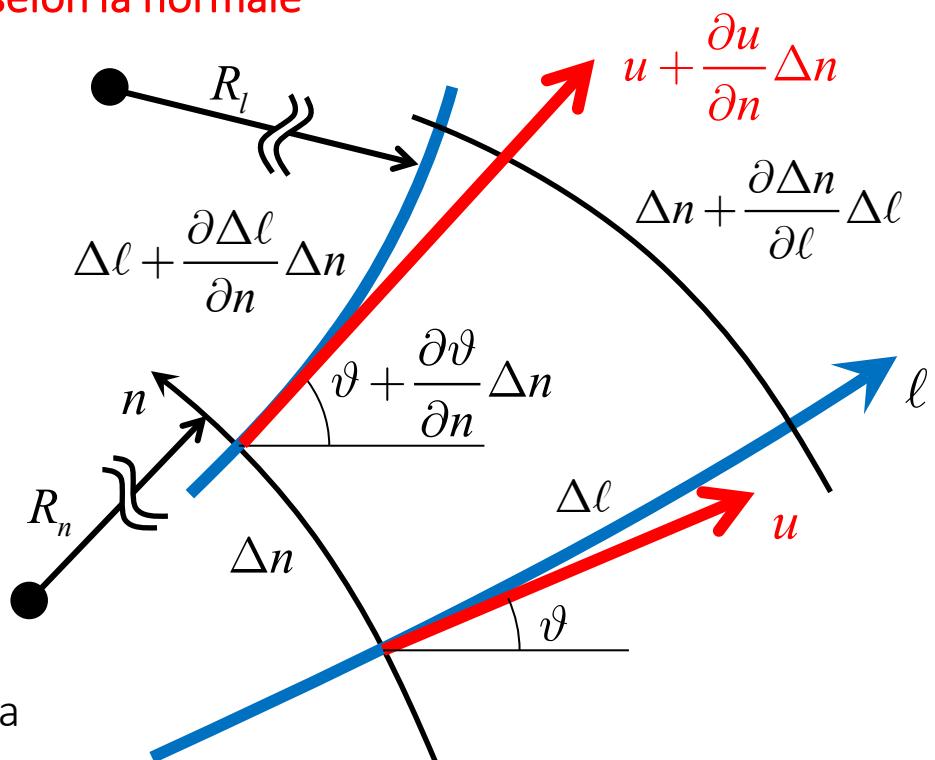


$$-\frac{\partial u}{\partial n} + u \frac{\partial \vartheta}{\partial \ell} = 0$$

- Conservation de la quantité de mouvement **selon la normale**

$$\frac{u^2}{R_l} = -\frac{1}{\rho} \frac{\partial p}{\partial n}$$

$$u^2 \frac{\partial \vartheta}{\partial \ell} = -\frac{1}{\rho} \frac{\partial p}{\partial n}$$



- On peut montrer qu'elle est **équivalente** à la conservation d'énergie et à la condition d'**irrotationnalité**

- Elle est donc superflue

$$\frac{1}{R_l} = -\frac{1}{\Delta \ell} \frac{\partial \Delta \ell}{\partial n} = \frac{\partial \vartheta}{\partial \ell}$$

- Etant données les nombreuses contraintes (homotropie, irrotationnalité, enthalpie totale constante, écoulement permanent, fluide non visqueux), deux équations suffisent pour décrire l'écoulement

$$-\frac{\partial u}{\partial n} + u \frac{\partial \vartheta}{\partial \ell} = 0$$

$$(M^2 - 1) \frac{1}{u} \frac{\partial u}{\partial \ell} - \frac{\partial \vartheta}{\partial n} = 0$$

- On introduit l'angle de l'onde de Mach μ

$$\tan \mu = \frac{1}{\sqrt{M^2 - 1}}$$

➤ On trouve alors

$$-\tan \mu \frac{\sqrt{M^2 - 1}}{u} \frac{\partial u}{\partial n} + \frac{\partial \vartheta}{\partial \ell} = 0$$

$$\frac{\sqrt{M^2 - 1}}{u} \frac{\partial u}{\partial \ell} - \tan \mu \frac{\partial \vartheta}{\partial n} = 0$$

$$-\frac{\partial u}{\partial n} + u \frac{\partial \vartheta}{\partial \ell} = 0$$

$$\tan \mu = \frac{1}{\sqrt{M^2 - 1}}$$

$$(M^2 - 1) \frac{1}{u} \frac{\partial u}{\partial \ell} - \frac{\partial \vartheta}{\partial n} = 0$$

➤ On rappelle la définition de la **fonction de Prandtl-Meyer**

$$d\nu = \sqrt{M^2 - 1} \frac{du}{u}$$

➤ On trouve alors

$$-\tan \mu \frac{\partial \nu}{\partial n} + \frac{\partial \vartheta}{\partial \ell} = 0$$

$$\frac{\partial \nu}{\partial \ell} - \tan \mu \frac{\partial \vartheta}{\partial n} = 0$$

➤ En soustrayant et en additionnant

$$\left(\frac{\partial}{\partial \ell} + \tan \mu \frac{\partial}{\partial n} \right) (\nu - \vartheta) = 0$$

$$\left(\frac{\partial}{\partial \ell} - \tan \mu \frac{\partial}{\partial n} \right) (\nu + \vartheta) = 0$$

- Soit une fonction $F(l, n)$

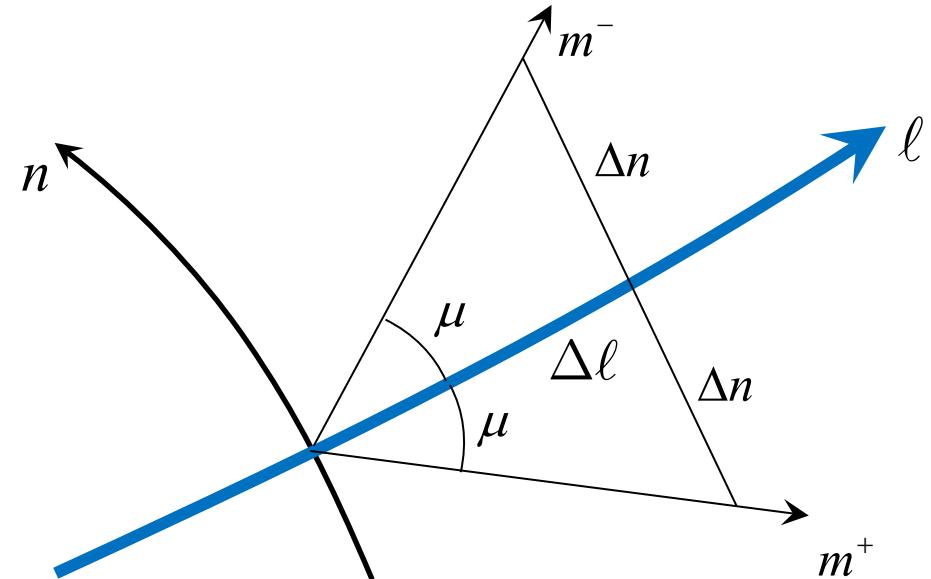
$$\frac{dF}{dm^-} = \frac{\partial F}{\partial \ell} \frac{\partial \ell}{\partial m^-} + \frac{\partial F}{\partial n} \frac{\partial n}{\partial m^-}$$

- Relations géométriques

$$\frac{d\ell}{dm^-} = \cos \mu \quad \frac{dn}{dm^-} = \sin \mu$$

$$\frac{dF}{dm^-} = \cos \mu \left(\frac{\partial F}{\partial \ell} + \tan \mu \frac{\partial F}{\partial n} \right)$$

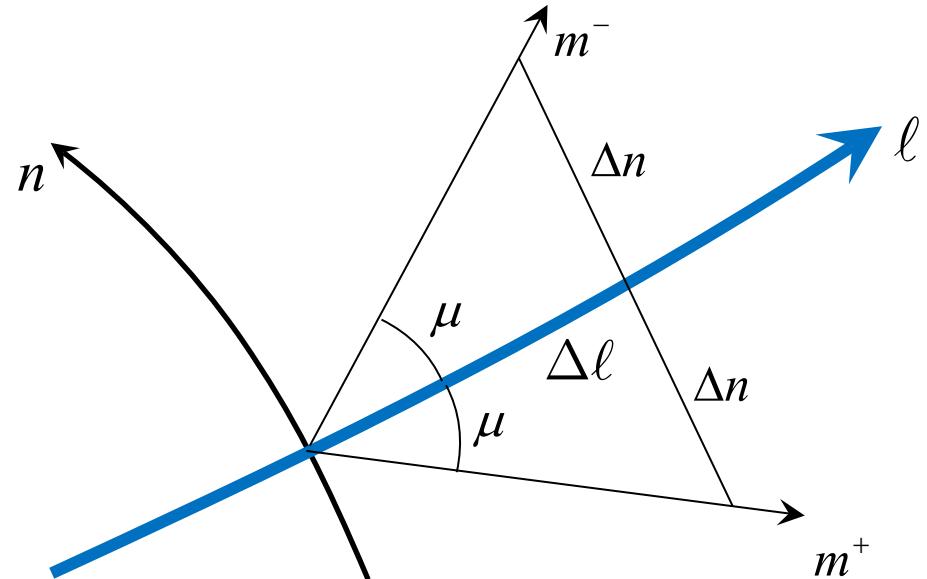
$$\frac{dF}{dm^+} = \cos \mu \left(\frac{\partial F}{\partial \ell} - \tan \mu \frac{\partial F}{\partial n} \right)$$



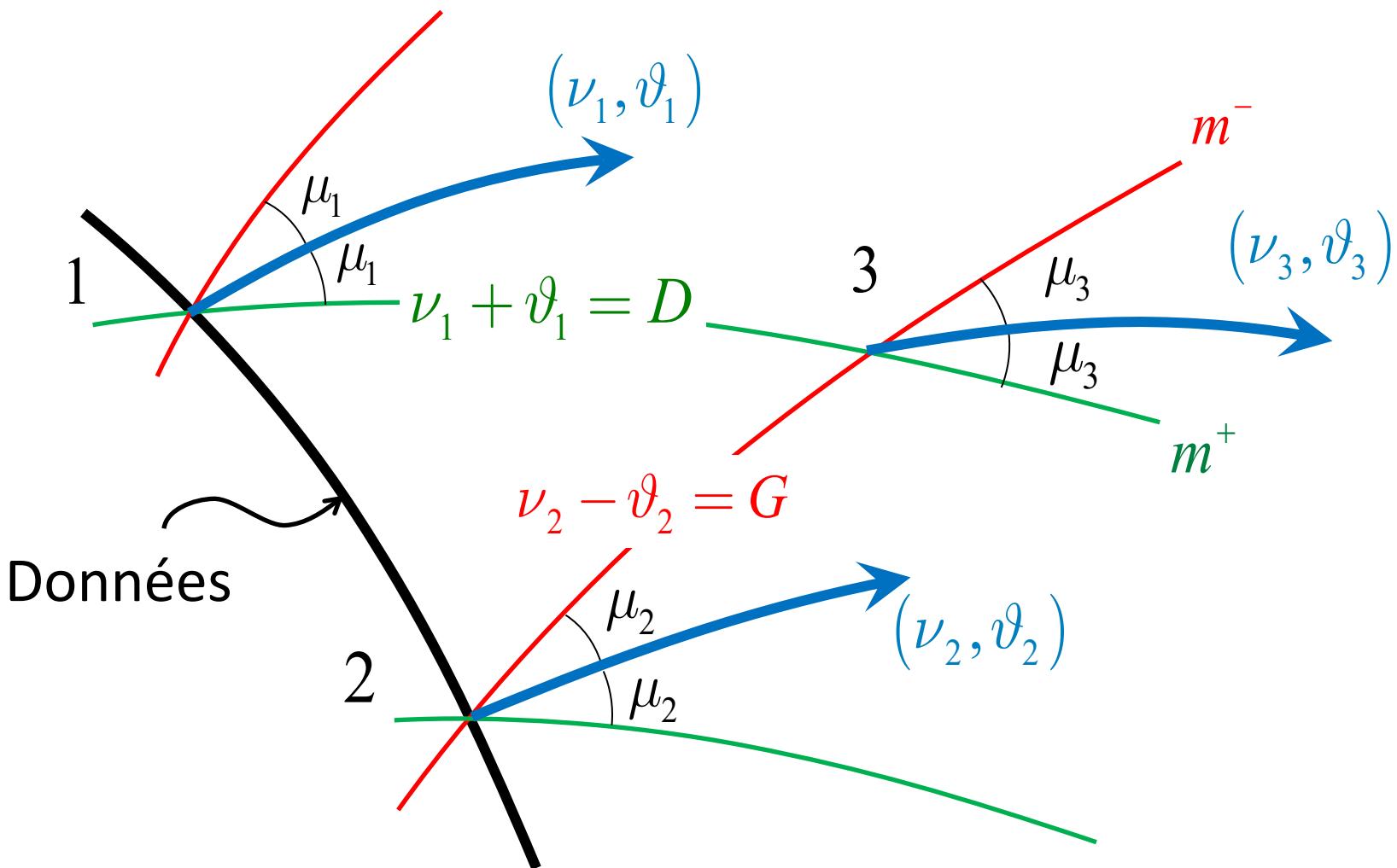
➤ On trouve alors

$$\frac{d}{dm^-}(\nu - \vartheta) = 0$$

$$\frac{d}{dm^+}(\nu + \vartheta) = 0$$

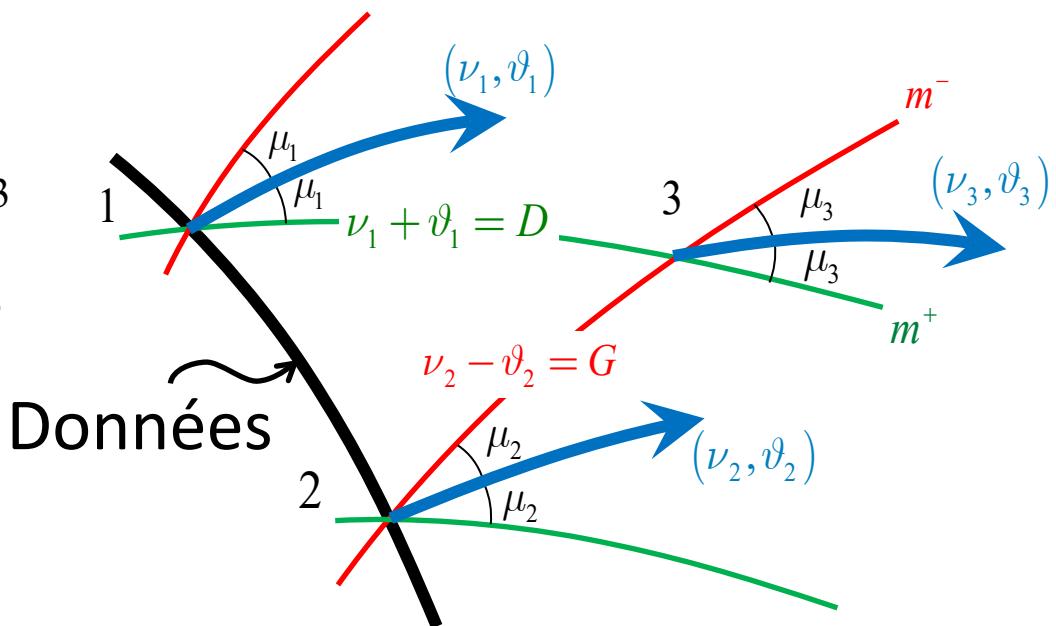


$\nu - \vartheta = const = G$	le long de la caractéristique	m^-
$\nu + \vartheta = const = D$	le long de la caractéristique	m^+



$$G_2 = \nu_2 - \vartheta_2 = G_3 = \nu_3 - \vartheta_3$$

$$D_1 = \nu_1 + \vartheta_1 = D_3 = \nu_3 + \vartheta_3$$



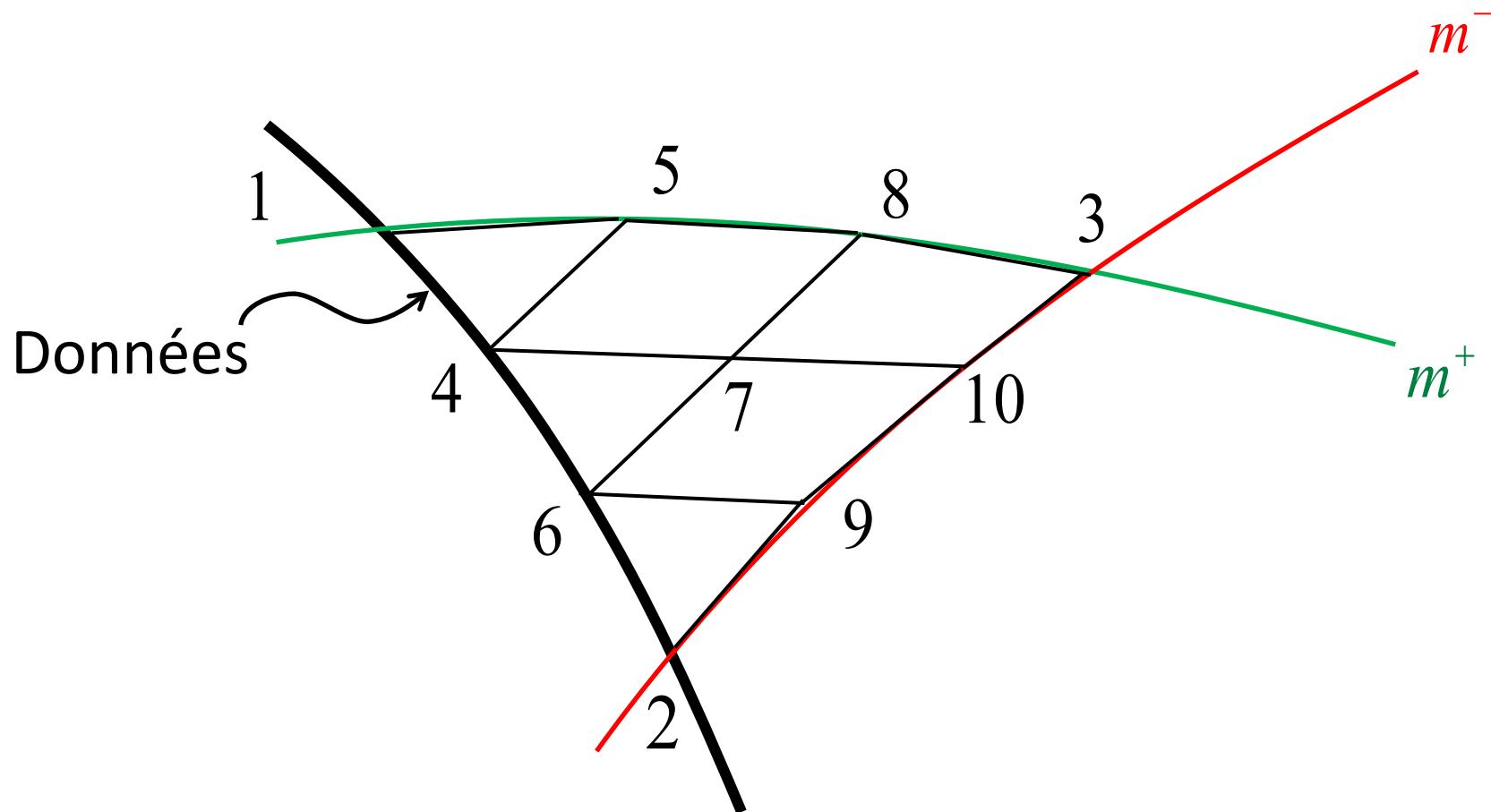
$$\nu_3 = \frac{1}{2}(\nu_1 + \nu_2) + \frac{1}{2}(\vartheta_1 - \vartheta_2)$$

$$\vartheta_3 = \frac{1}{2}(\nu_1 - \nu_2) + \frac{1}{2}(\vartheta_1 + \vartheta_2)$$

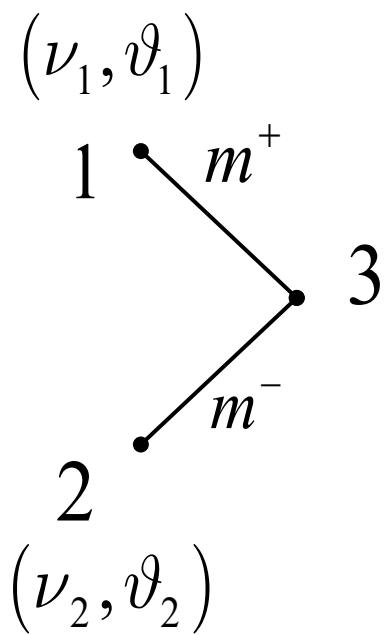
$$\nu = \frac{1}{2}(D + G)$$

$$\vartheta = \frac{1}{2}(D - G)$$

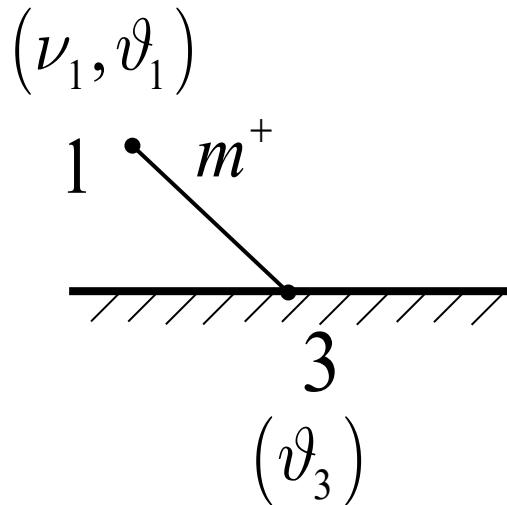
- Problème: on ne connaît pas a priori les caractéristiques!



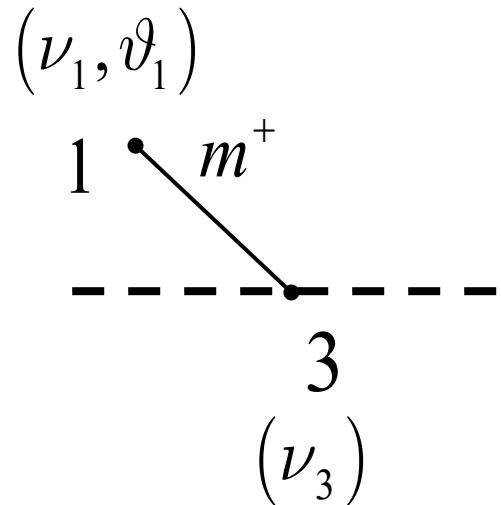
➤ Point intérieur



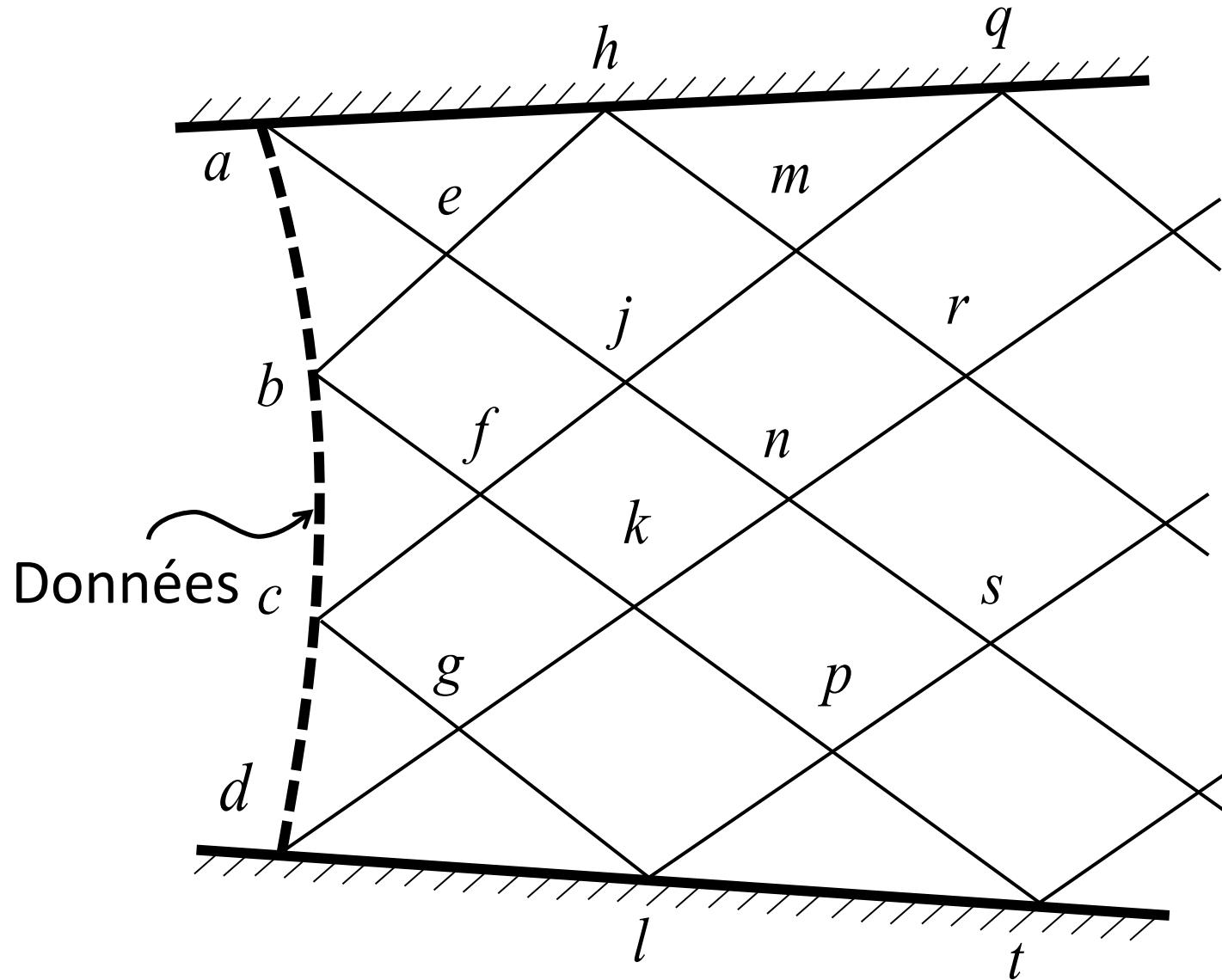
➤ Paroi



➤ Surface libre

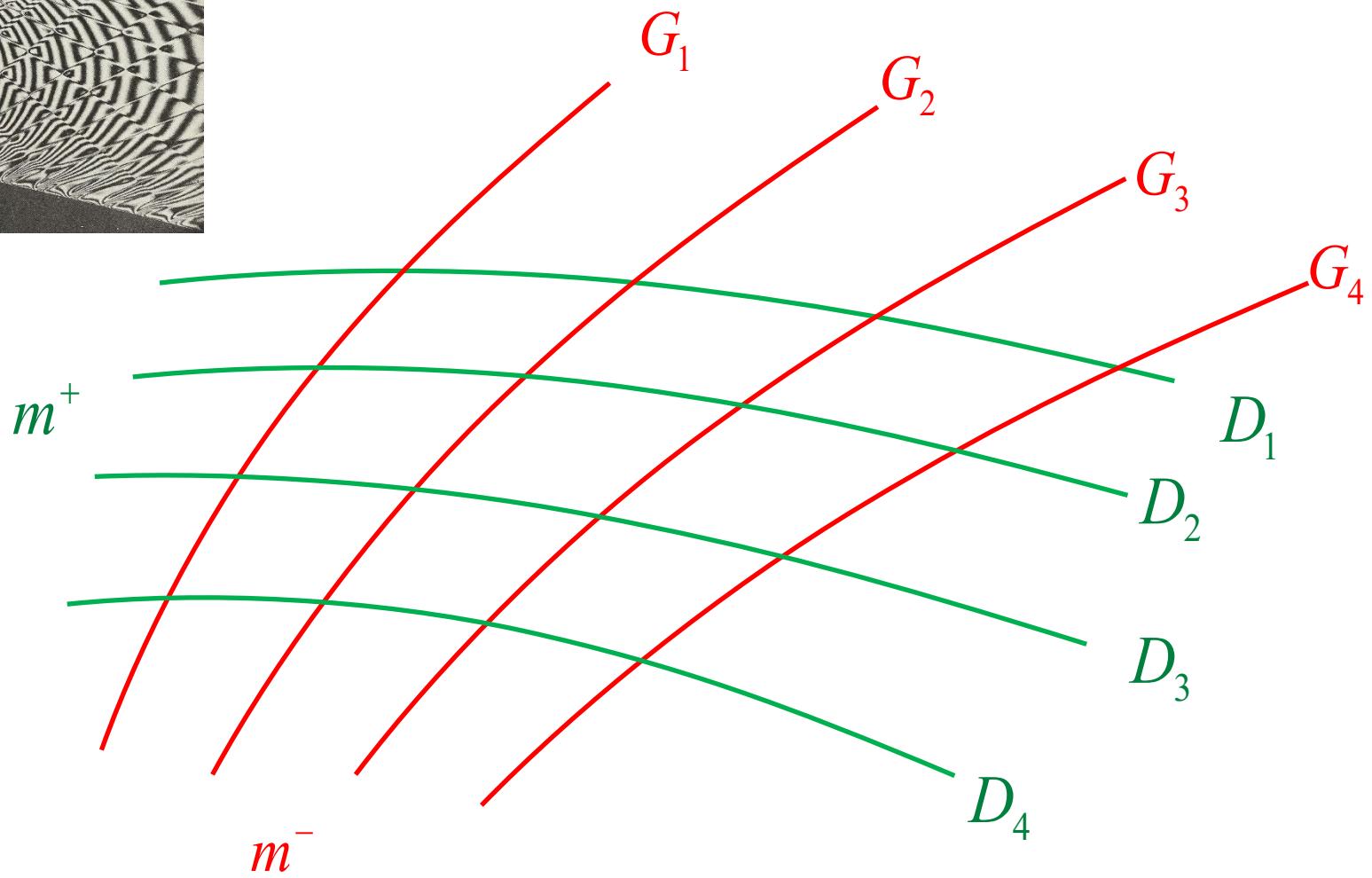
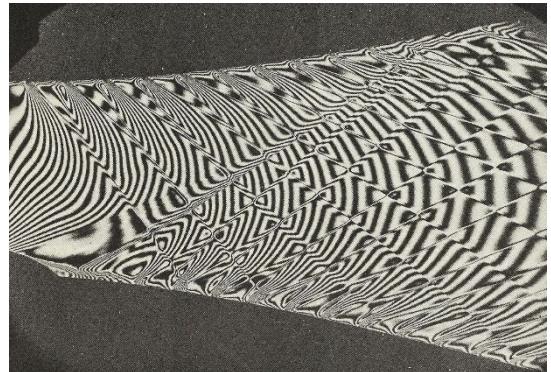


Tuyère supersonique

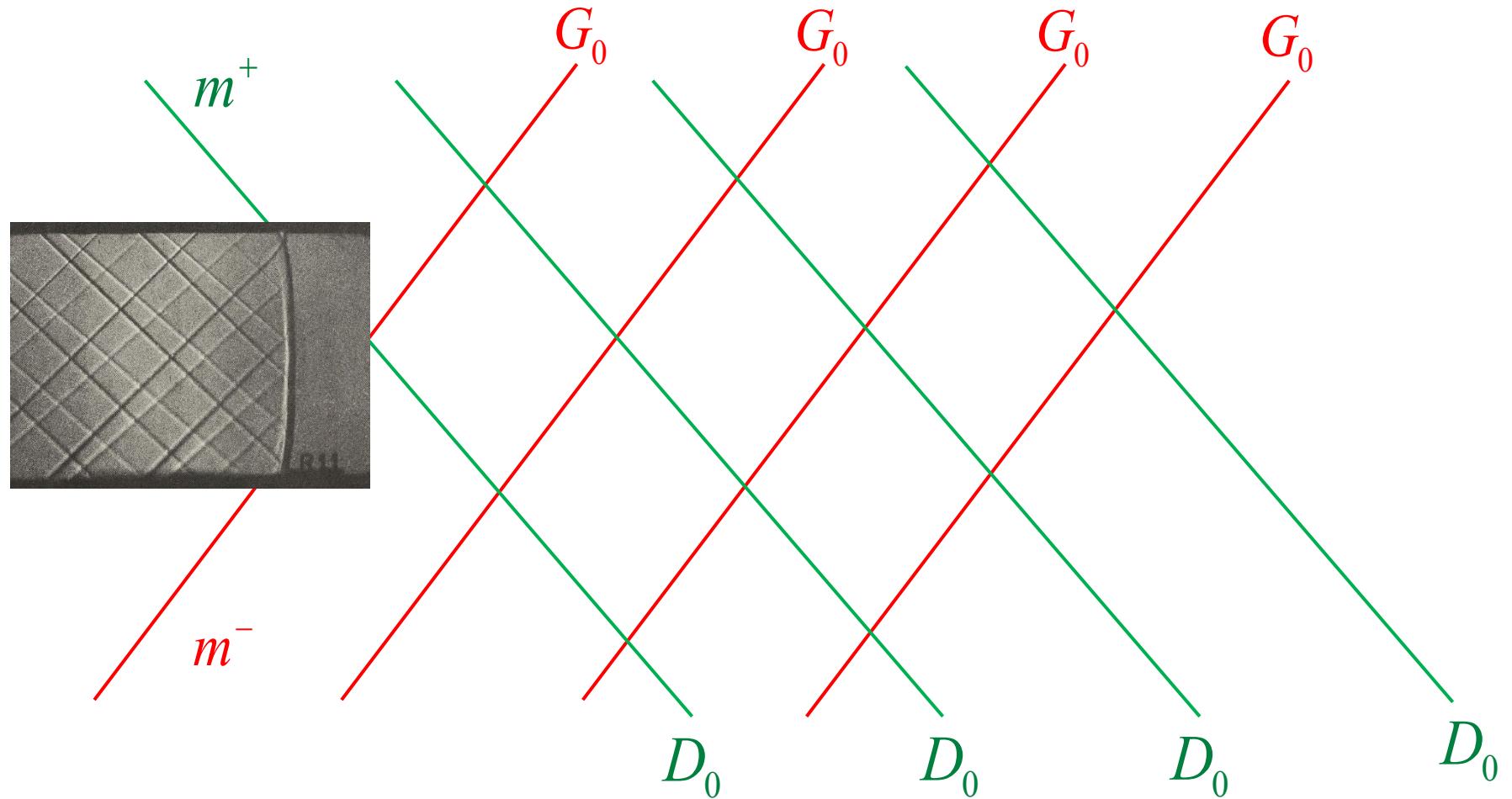


Région non simple

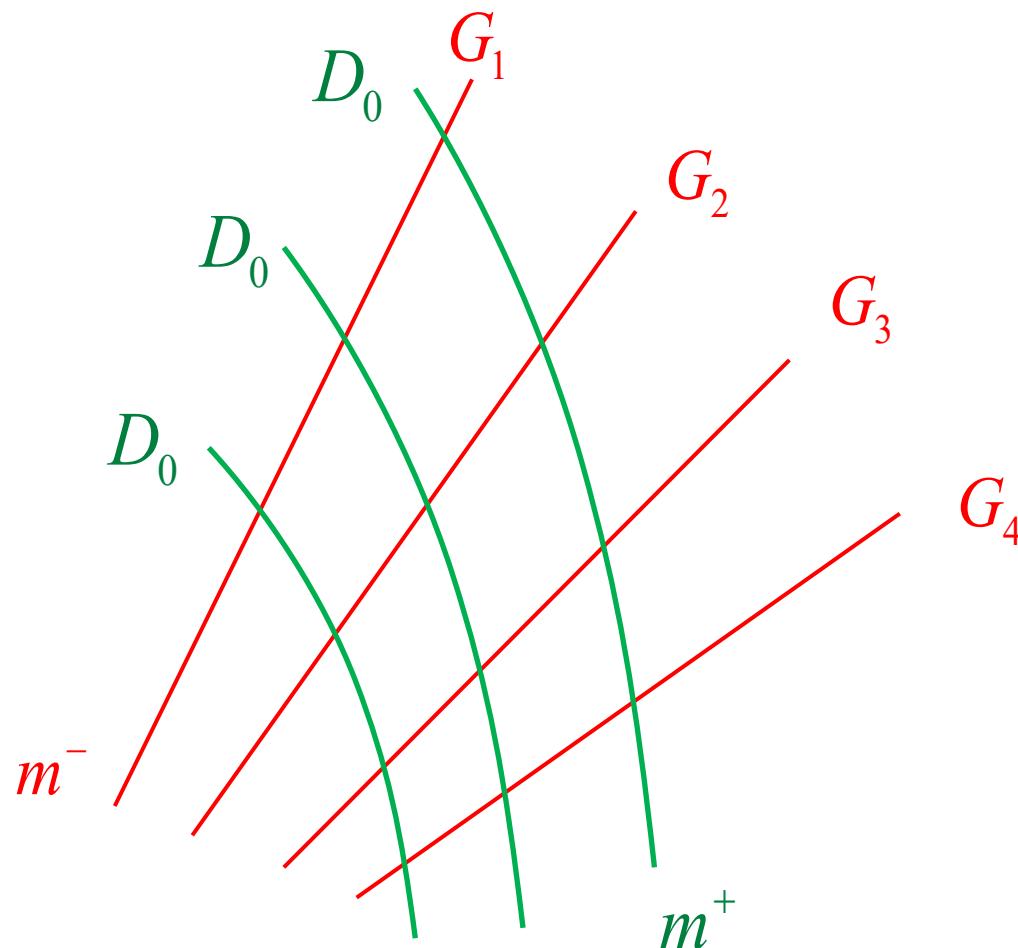
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Région uniforme



Région simple



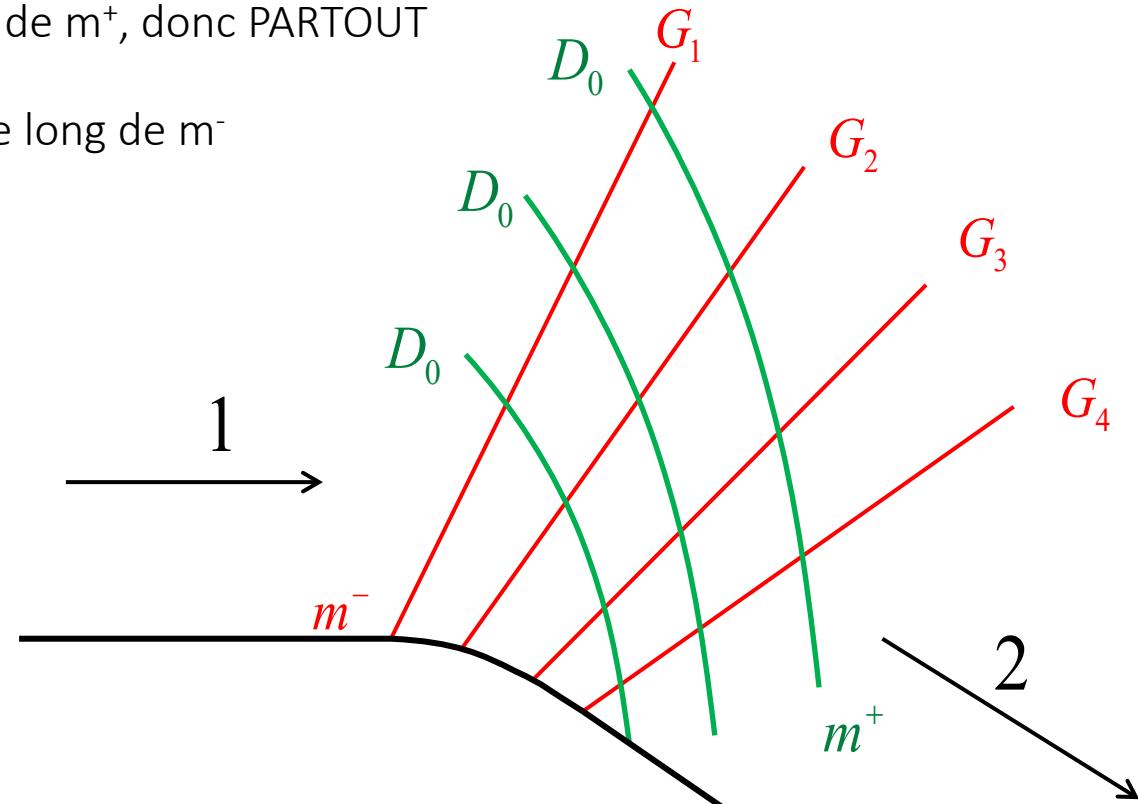
$\vartheta + \nu = \nu_1 = \nu(M_1)$ le long de m^+ , donc PARTOUT

$\vartheta - \nu = const = 2\vartheta - \nu_1$ le long de m^-

➤ Donc, le long de m^-

$\vartheta = const$

$\nu = \nu_1 - \vartheta = const$



➤ Les caractéristiques m^-
sont des lignes droites

$$\vartheta = \text{const}$$

le long de m^-

$$\nu = \nu_1 - \vartheta = \text{const}$$

➤ Méthode de résolution:

- On commence par G_1
- On évalue ϑ (= angle de la paroi)
- On évalue $\nu = \nu_1(M_1) - \vartheta$
- On évalue M (à partir de $\nu(M)$)
- On évalue l'angle de Mach μ à partir du nombre de Mach
- On évalue l'angle de la caractéristique G_1 $\vartheta + \mu$
- On recommence avec G_2

